

FormulaEs

$$\text{Sneddon's: } hc = h_{\max_{\text{corr}}} - \varepsilon (P_{\max} / S)$$

Projected Area of Contact at the contact depth (hc): $Ap = a_0 hc^2 + a_1 hc$
 Example: $a_0 = 24.56$ for ideal Berkovich or Vickers Indenters ; a_1 is for tip rounding

Reduced Elastic Modulus: $E_R = (S_{h_{\max}} \sqrt{\pi}) / (2 \sqrt{Ap})$
 note: The $S_{h_{\max}}$ is the slope at the maximum depth for the indentation.

$$\text{Elastic Modulus of Sample: } E_s = (1 - V_s^2) / ((1 / E_R) - ((1 - V_i^2) / E_i))$$

$$\text{Poisson's Ratio of Sample: } V_s = \sqrt{(1 - E_s (1 / E_R - (1 - V_i^2) / E_i))}$$

Load: $P = \alpha (h - h_f)^m$ newline newline

Slope(dP/dh): $S = \alpha m (h - h_f)^{(m - 1)}$ newline newline

Machine Compliance Correction Factor (Cf): $h_{\text{corr}} = h_i - C_f P_i$ newline newline

Sneddon's: $hc = h_{\max_{\text{corr}}} - \varepsilon (P_{\max} / S)$ newline newline

Projected Area of Contact at the contact depth (hc): $Ap = a_0 hc^2 + a_1 hc$ newline
 Example: $a_0 = 24.56$ for ideal Berkovich "or" Vickers Indenters; a_1 is for tip rounding newline newline

Reduced Elastic Modulus: $E_R = (S_{h_{\max}} \sqrt{\pi}) / (2 \sqrt{Ap})$ newline
 note: The $S_{h_{\max}}$ is the slope at the maximum depth for the indentation. newline newline

Elastic Modulus of Sample: $E_s = (1 - V_s^2) / ((1 / E_R) - ((1 - V_i^2) / E_i))$ newline newline

Poisson's Ratio of Sample: $V_s = \sqrt{(1 - E_s (1 / E_R - (1 - V_i^2) / E_i))}$ newline newline

Elastic Modulus of Indenter: $E_i = (1 - V_i^2) / ((1 / E_R) - ((1 - V_s^2) / E_s))$ newline newline

Poisson's Ratio of Indenter: $V_i = \sqrt{(1 - E_i (1 / E_R - (1 - V_s^2) / E_s))}$ newline newline